# Development of wind tunnel and numerical simulations for the flow around a circular cylinder over a large range of Reynolds numbers 

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#### Abstract

SUMMARY: For the design of high-rise buildings or other slender structures wind effects such as wind loading and dynamic behaviour become relevant for the design. Wind tunnel or numerical simulations are the two methods currently available to model the behaviour. For the occurring very high Reynolds numbers both methods are limited and the models are usually scaled down. While this is acceptable for sharp edged shapes the prediction of the flow behaviour for rounded shapes still poses a challenge. As numerical simulations improve with increasingly available computational power they might close this gap in the future. In order to judge both developments an extensive literature review for the basic circular cylinder is undertaken. For wind tunnel and numerical simulations a large range of results is documented for the critical transition of the flow, where the behaviour is highly dependent on the surface roughness. To go beyond this range the lack of existing reference data makes a validation even more complex. This paper focusses on the comparison of wind tunnel and numerical simulations for the flow around the circular cylinder in the scientific research community.


Keywords: high-rise buildings, CFD, slender structure, circular cylinder, surface roughness, accuracy

## 1. INTRODUCTION

For safe and sustainable slender structures it is important to accurately predict the wind loads and the dynamic behaviour in turbulent flow. While constructions with sharp edges can be scaled, the flow around high-rise buildings with rounded corners, chimneys or wind-turbine towers is highly dependent on the Reynolds number. As very high Reynolds numbers (up to $10^{7}$ and $10^{8}$ ) can occur, the state of the art wind tunnel approach with scaled models reaches a limit for rounded building-shapes. So far advancing Computational Fluid Dynamics (CFD) applications have also been limited to smaller Reynolds numbers as the required computational power increases with higher numbers. However, with gradually increasing computational power, the boundaries and accuracy of CFD are developing with technological advances. The questions arise to which extend the accuracy increases and what data to use for validation.
To judge the accuracy of models, it is essential to ensure a correct depiction of the physical behaviour. Due to its dependence on the turbulence intensity, mixing length, dimension of the object, surface roughness and the Reynolds number, the flow around rounded shapes is complex. The basic circular cylinder has been studied intensively throughout different disciplines and methods for around a century creating a large data base of published results. This makes the circular cylinder particularly suitable for the overview regarding the development of wind tunnel tests and CFD sim-
ulations over time and Reynolds number. The current research also includes CFD simulations to further study the limits and influencing factors of the simulations throughout the different Reynolds numbers.

## 2. METHODOLOGY

Existing literature on the circular cylinder from the beginning of wind tunnel testing until now is summarized. Comparable values such as the drag and lift coefficient, the Strouhal number and the pressure coefficients over the surface are compiled as a reference. In OpenFOAM the air flow ( $\rho=1 \mathrm{~kg} / \mathrm{m}^{3}$ and $v=1.5 \cdot 10^{-5} \mathrm{~m}^{2} / \mathrm{s}$ ) around a circular building cross-section of 30 m diameter is simulated for gradually increasing velocities up to $50 \mathrm{~m} / \mathrm{s}$ (Mach number $<0.2$, incompressible, $\operatorname{Re}=10^{8}$ ). For the URANS (unsteady Reynolds averaged Navier Stokes) simulations the k- $\varepsilon$ and $\mathrm{k}-\omega$ SST turbulence models are applied. A domain size of $600 \mathrm{~m}(20 \mathrm{~d})$ towards the inlet, top and bottom and $1800 \mathrm{~m}(60 \mathrm{~d})$ towards the outlet is modelled with a block mesh for which mesh independence is ensured. The cylinder surface is smooth, the turbulence intensity $5 \%$ and the mixing length / diameter ratio $10 \%$. The simulation time is set to ensure that the fluid flows through the domain at least 3 times and the Courant number is below $<1$.

## 3. RESULTS

In figure 1 some of the results for the mean drag coefficient are displayed over the Reynolds number. The critical transition range is zoomed in the lower subfigure. Recently published results from literature are displayed with an increasing visual impact: wind tunnel simulations (grey), CFD simulations (blue), full-scale measurements (purple), DIN EN 1991-1-4, 2010 (black). When the surface roughness is stated and altered the results are grouped into the categories of the DIN EN 1991-1-4, 2010 and indicated with the equivalent line. Own simulation results according to section 2 are marked in red.
It can be seen that CFD simulations develop towards higher Reynolds numbers and can reproduce the drop in the drag coefficient around the critical flow transition to a certain extend. While wind tunnel and numerical simulations align rather well for the Reynolds numbers up to the Kármán vortex street, the range of results in the transition phase, with the high dependency on the boundary conditions, is large. Published results often miss precise information regarding those influencing factors, which is essential for validation. A lack of reliable data for very high Reynolds numbers becomes evident. The simulations of this study confirm the high accuracy for Reynolds numbers towards the subcritical range and the need for further studies for the transition phase.

## 4. CONCLUSION

Until the transition range of the flow around a circular cylinder wind tunnel experiments and numerical simulations mostly align. In order to judge the accuracy in the transition range the research has to be extended regarding an evaluation of specific conditions for published results and own studies. Even though numerical simulation progress to higher Reynolds numbers, significantly more studies are required for the transcritical Reynolds numbers in order to be able to validate the results. One approach is the bluff body benchmark by Breitkopf et al., 2022 that targets this range.


Figure 1. drag coefficient for circular cylinder over different Reynolds number obtained from CFD simulations or wind tunnel experiments between 1920 and today (flow characterisation at the top according to Schlichting and Gersten, 2006)

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